

## Figure Captions

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Fig. 2. Schematic illustration of a shell & tube type heat exchanger.

Fig. 3. Experimental system.

(a) Photograph of experimental system

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Fig. 12. Relation between non-dimensional tube length and bulk mean temperature.

(a)  $0 \leq L/L_T \leq 40$

(b)  $0 \leq L/L_T \leq 5$

Fig. 13. Relation between non-dimensional tube length and difference in specific enthalpy.

(a)  $0 \leq L/L_T \leq 40$

(b)  $0 \leq L/L_T \leq 5$

Fig. 14. Comparison of experiments and Eq. (6).

Fig. 15. Comparison of experiments and Eq. (7).

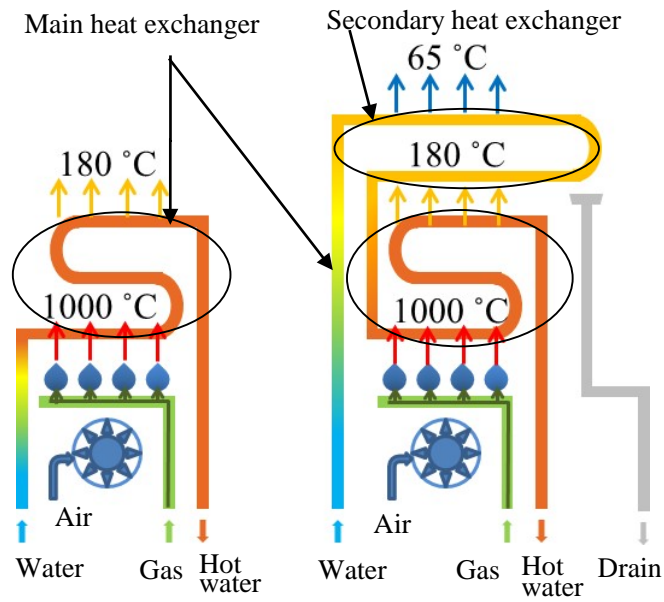
Fig. 16. Dimensional standard of configuration for proposed heat exchanger performance.

Fig. 17. Variation of pressure loss against effective tube length for moist air.

## Table Captions

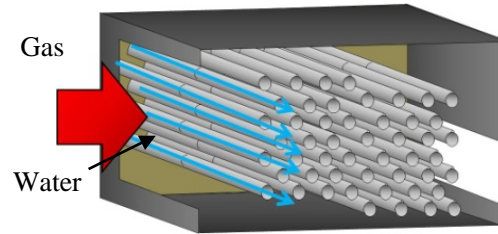
Table 1. Experimental conditions.

Table 2. Comparison of heat exchange volumes calculated by Eqs. (6) and (7).

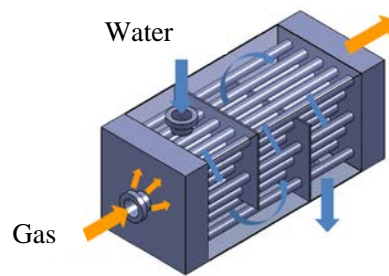


(a) Without secondary heat exchanger    (b) With secondary heat exchanger

Fig. 1. Water heater systems.

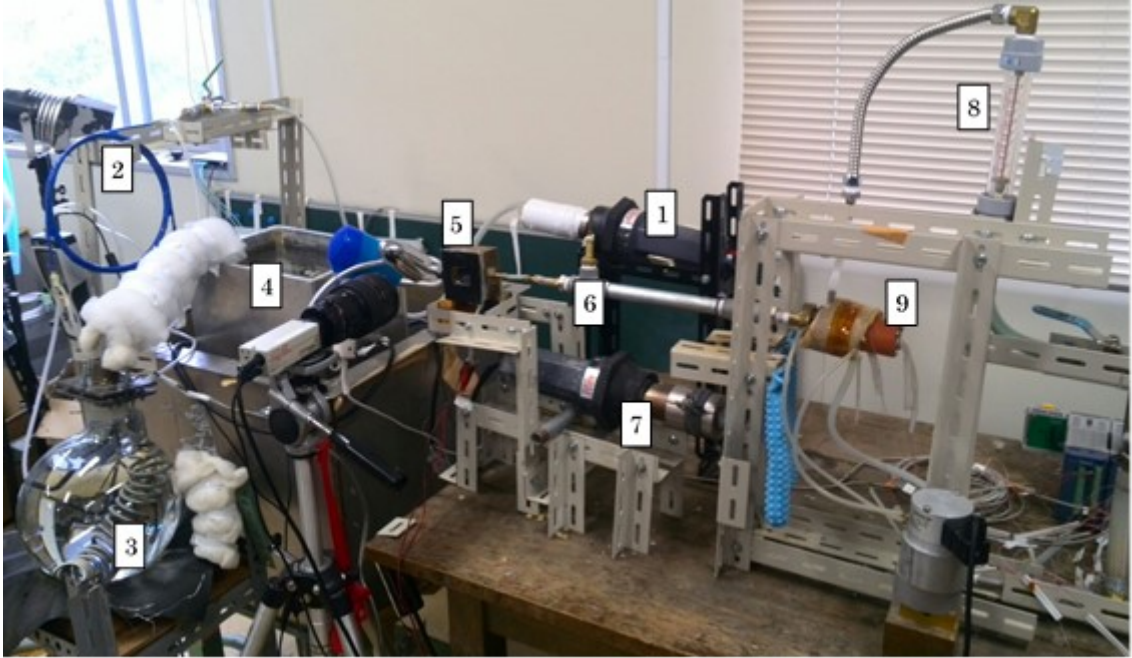


(a) Conventional type

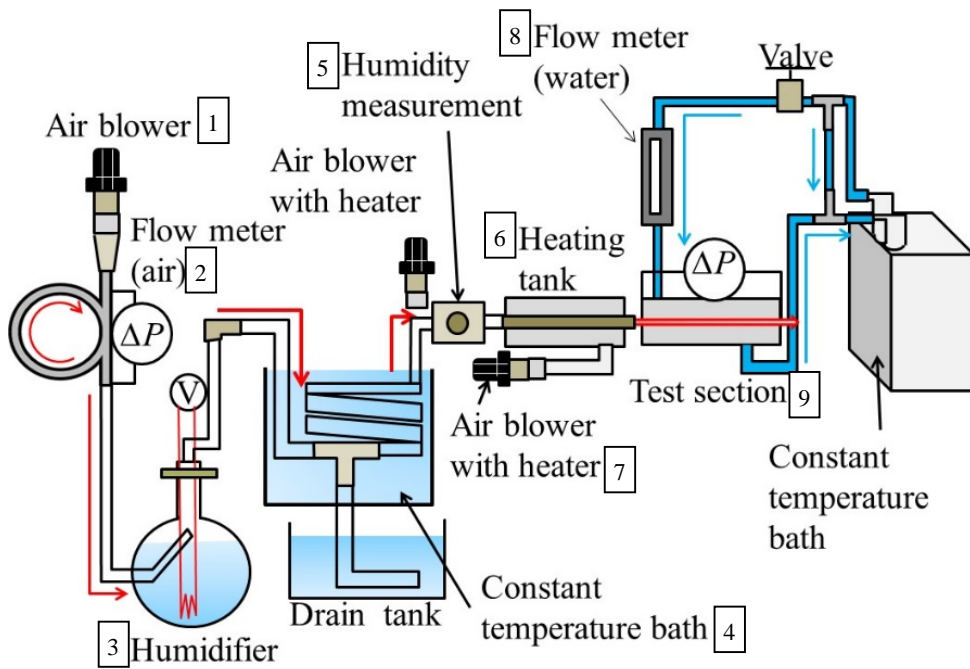


(b) Proposed type

Fig. 2. Schematic illustration of a shell & tube type heat exchanger.



(a) Photograph of experimental system



(b) Schematic of experimental system

Fig. 3. Experimental system

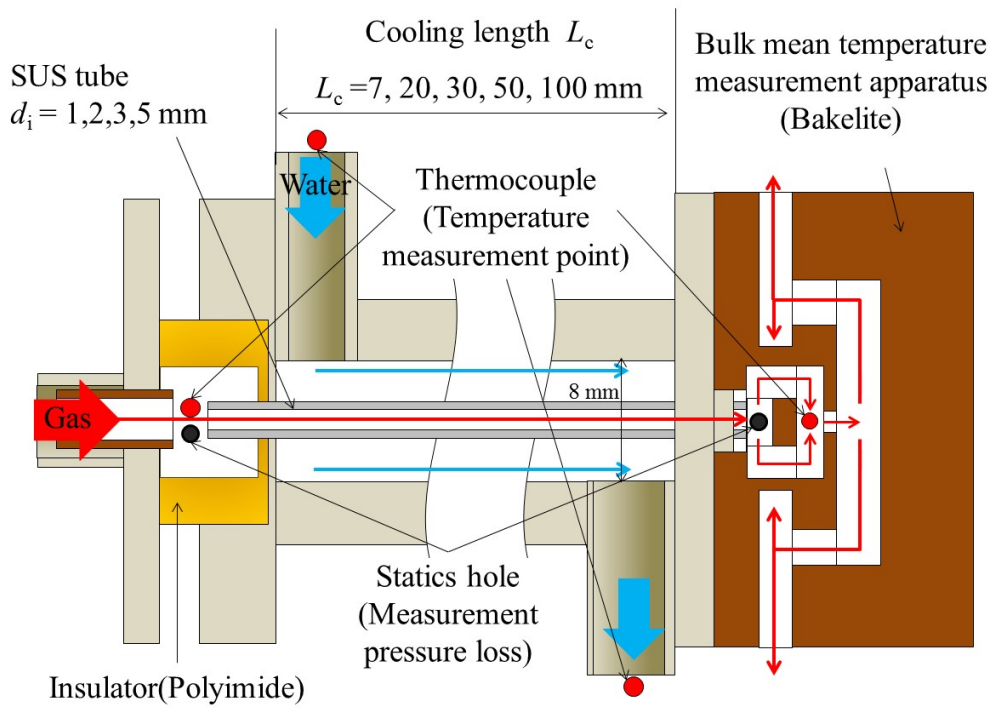
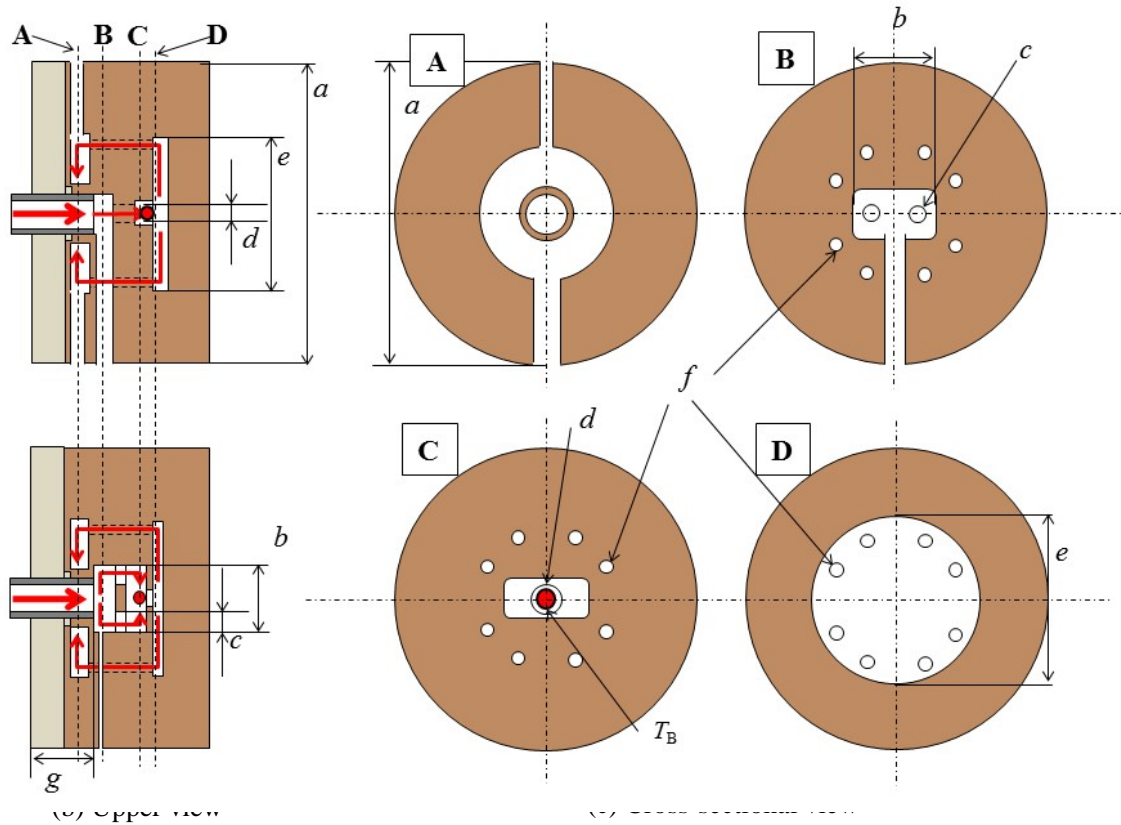


Fig. 4. Details of test section.



(d) Dimensions of apparatus

$d_i$ (mm)	$a$ (mm)	$b$ (mm)	$c$ (mm)	$d$ (mm)	$e$ (mm)	$f$ (mm)	$g$ (mm)
1.0, 2.0	45	7	1	1	20	0.8	3
3.0, 5.0		14	2.5	2.5		1.6	

Fig. 5. Details of bulk mean temperature measurement apparatus.

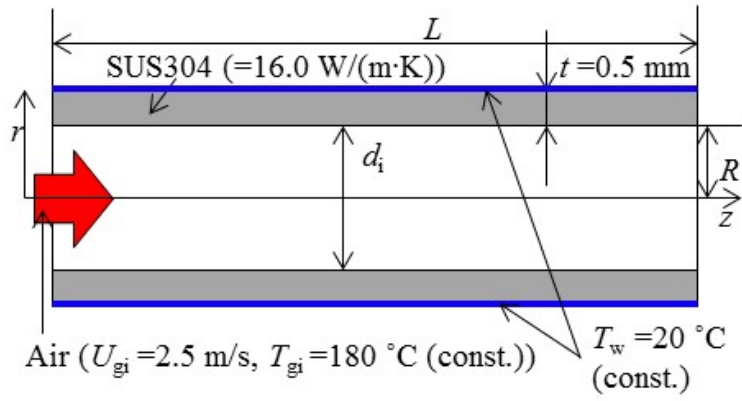


Fig. 6. Calculation model.

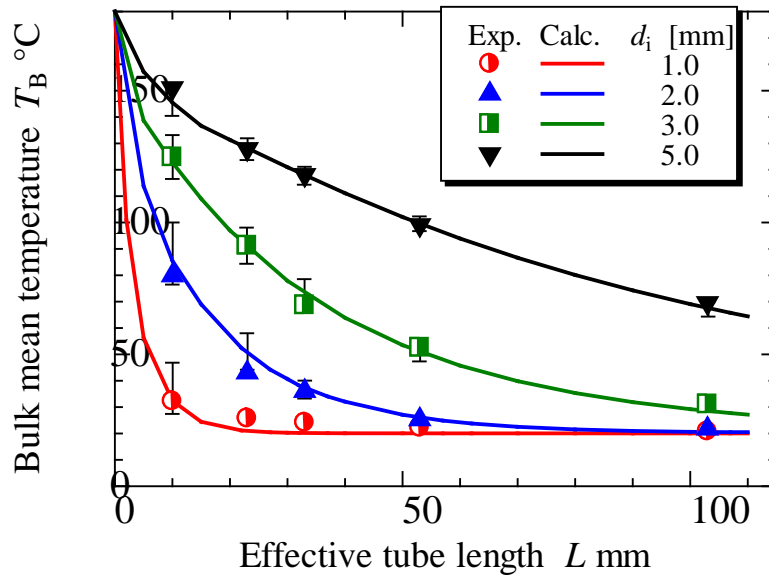


Fig. 7. Variation of bulk mean temperature against effective tube length for dry air.

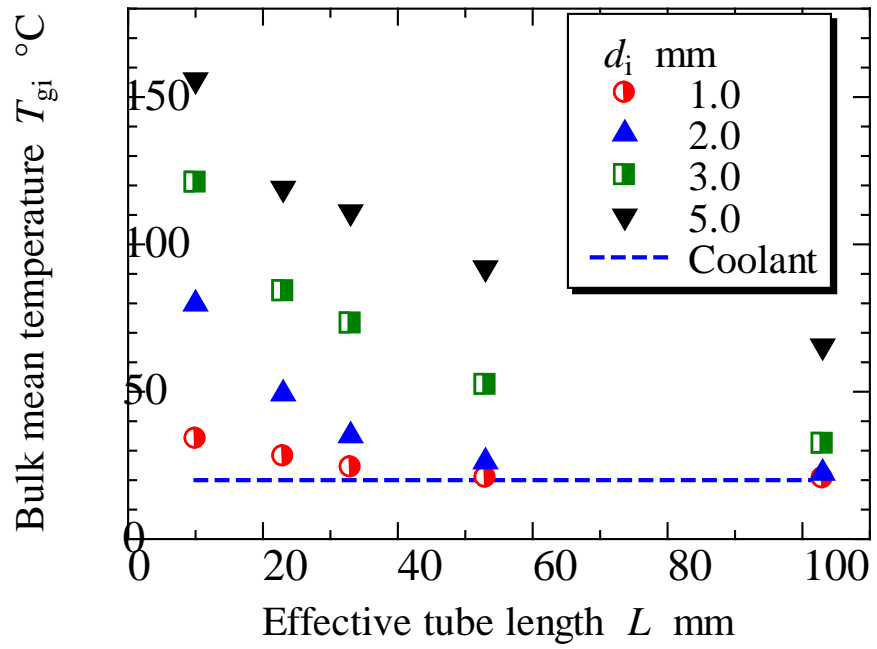


Fig. 8. Variation of bulk mean temperature against effective tube length for moist air.



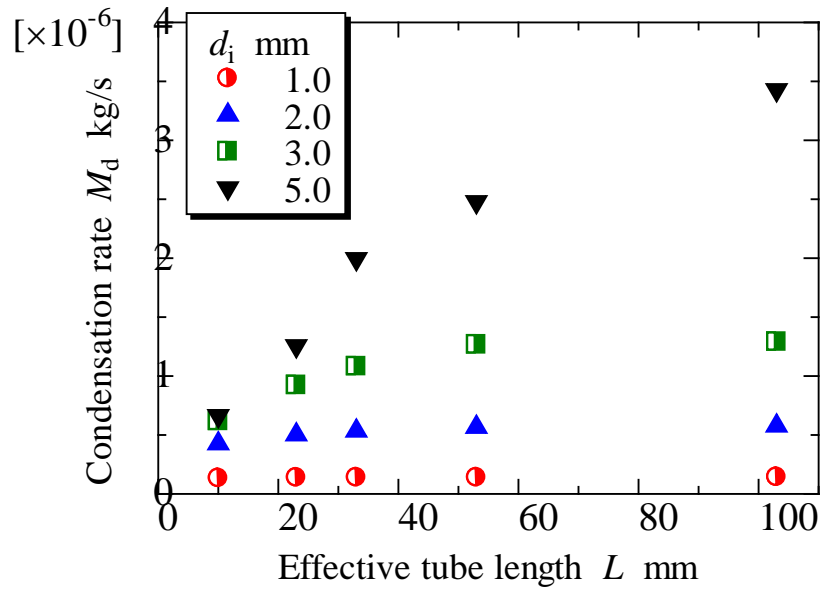


Fig. 9. Variation of condensation rate against effective tube length.

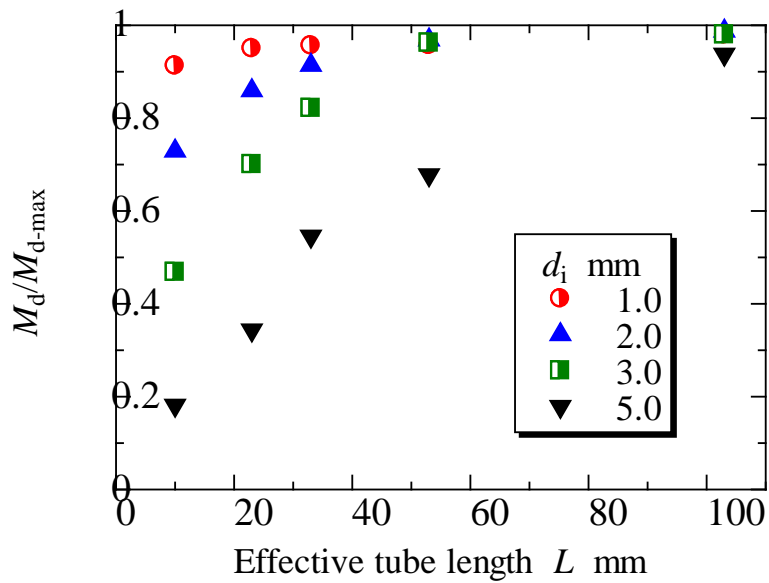


Fig. 10. Ratio of condensation rate to total humidity in gas flow.

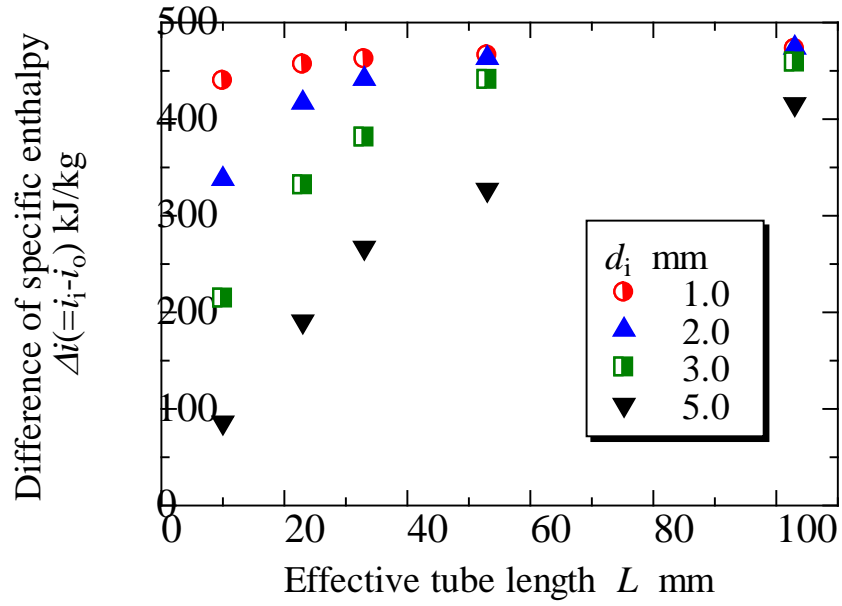
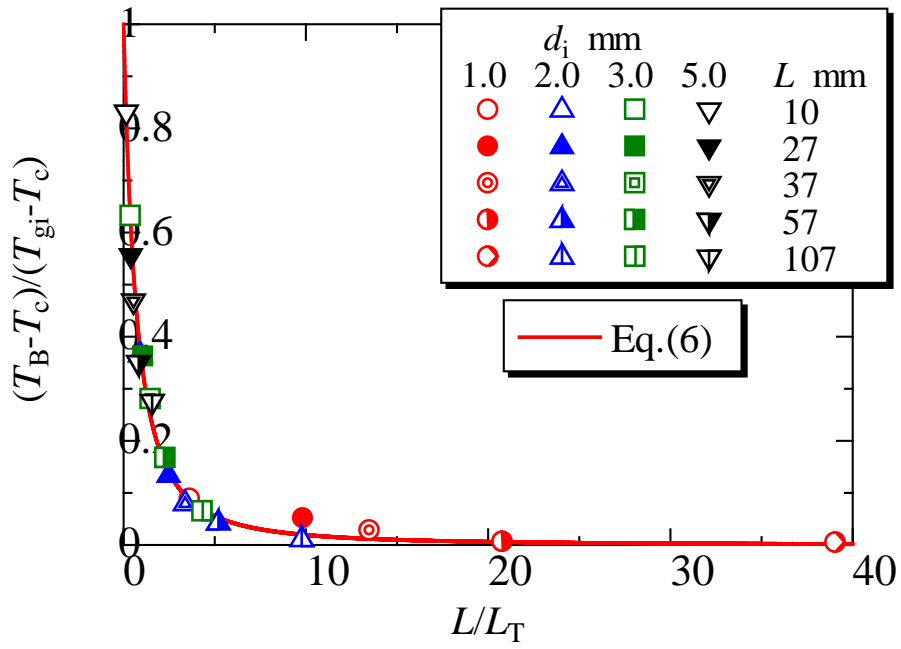
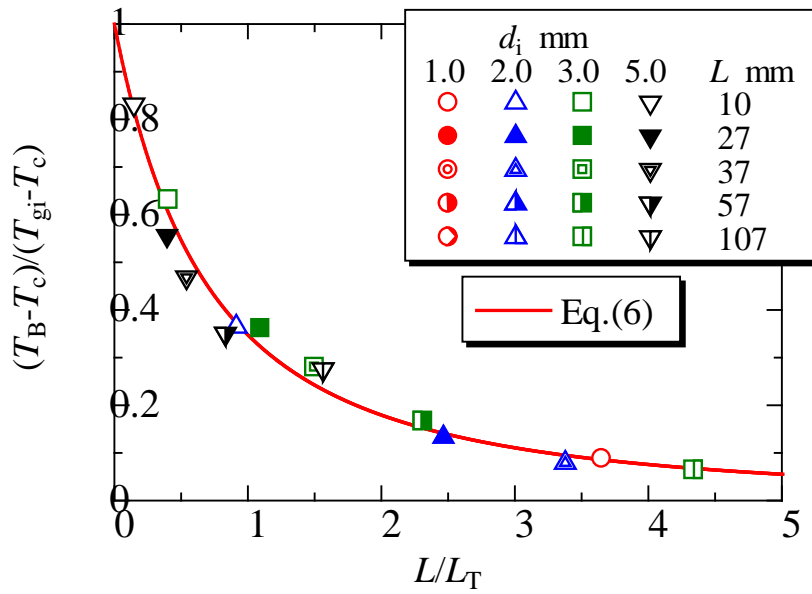


Fig. 11. Difference in specific enthalpy against effective tube length.

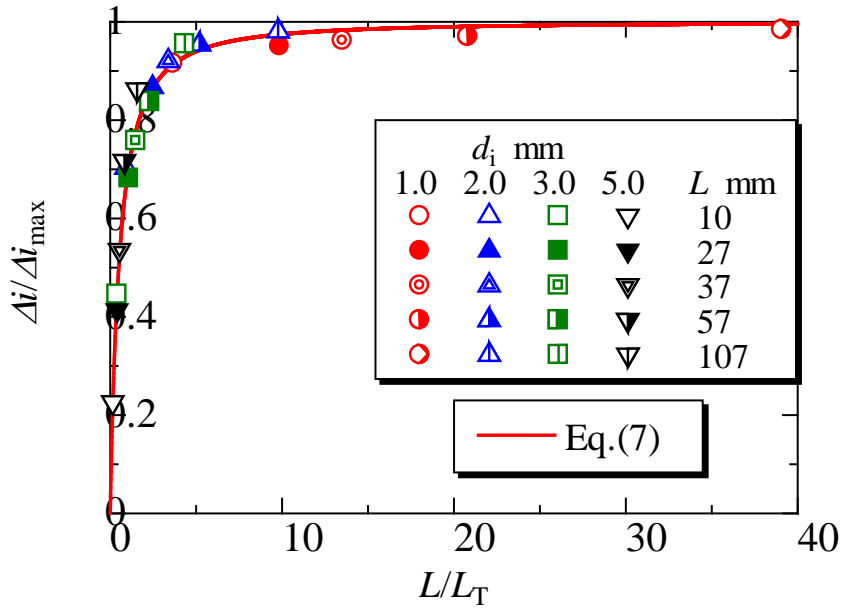


(a)  $0 \leq L/L_T \leq 40$

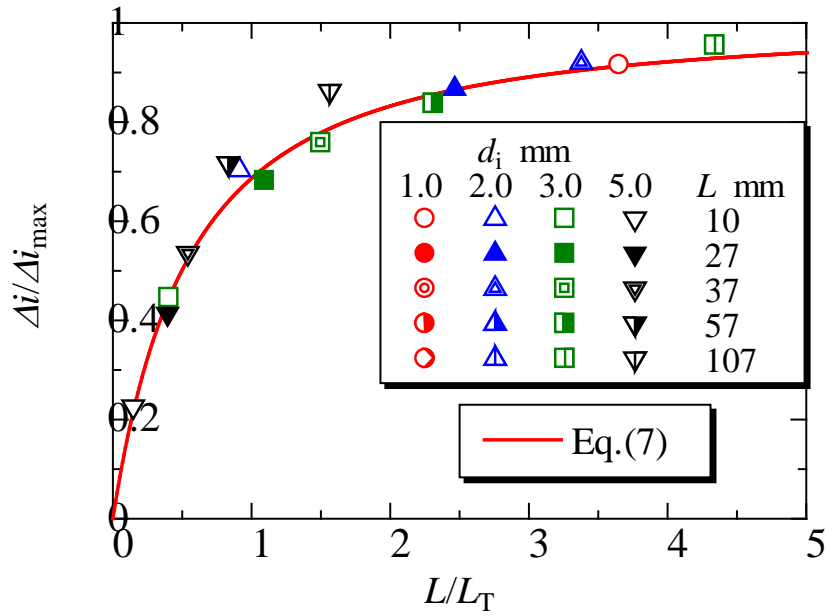


(b)  $0 \leq L/L_T \leq 5$

Fig. 12. Relation between non-dimensional tube length and bulk mean temperature.



(a)  $0 \leq L/L_T \leq 40$



(b)  $0 \leq L/L_T \leq 5$

Fig. 13. Relation between non-dimensional tube length and difference in specific enthalpy.

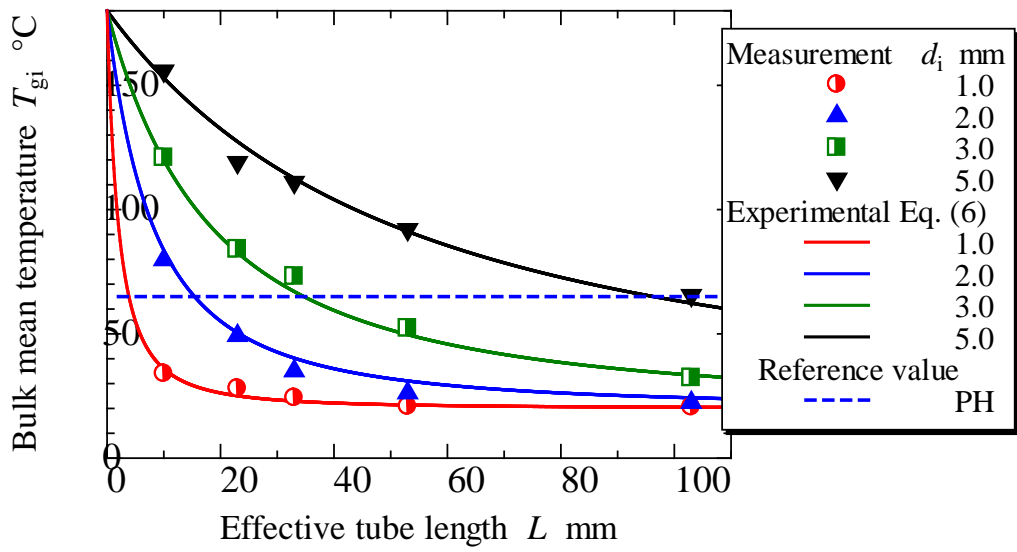


Fig. 14. Comparison of experiments and Eq. (6).

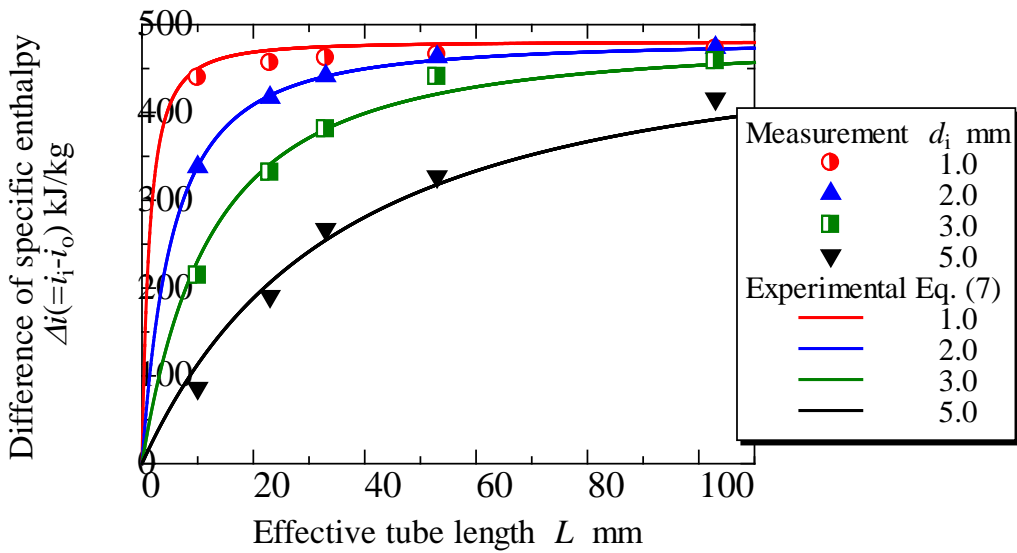


Fig. 15. Comparison of experiments and Eq. (7).

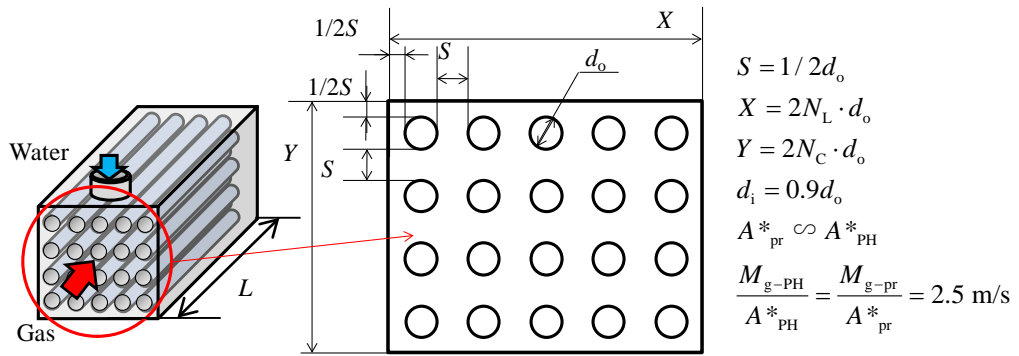


Fig. 16. Dimensional standard of configuration for proposed heat exchanger

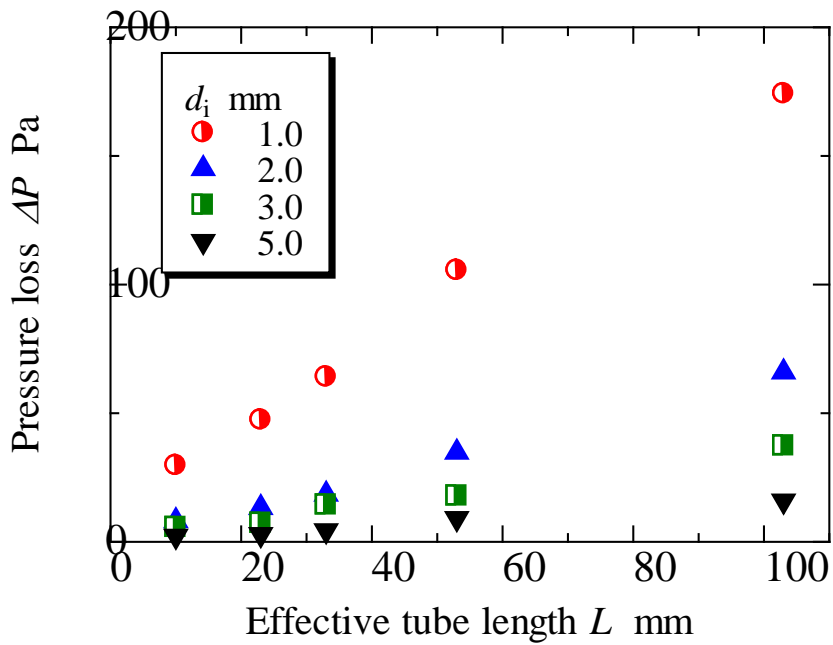


Fig. 17. Variation of pressure loss against effective tube length for moist air.

Table 1. Experimental conditions.

		Present study	PH
Gas		Humid air	City gas
	Material	SUS304	SUS316L
	Cooling length $L_c$ [mm]	7, 20, 30, 50, 100	105
Tube	Tube length [mm]	12, 25, 35, 55, 105	300
	Thickness $t$ [mm]	0.5	0.3
	Inner diameter $d_i$ [mm]	1.0, 2.0, 3.0, 5.0	5.4
	Velocity $U_g$ [m/s]	2.5	2.5
Gas	Inlet temperature $T_{gi}$ [°C]	180	180
	Specific humidity $x$ [kg/kg]	0.11	0.11
	Mass flow rate $M_g$ [kg/s]	1.5, 5.9, 13.5, 37.5 ( $\times 10^{-6}$ )	0.028
	Velocity $U_c$ [m/s]	1.2	1.2
Coolant	Inlet temperature $T_{ci}$ [°C]	20	20
	Mass flow rate $M_c$ [kg/s]	5.8, 5.0, 4.2, 2.5 ( $\times 10^{-2}$ )	0.22

Table 2. Comparison of heat exchange volumes calculated by Eqs. (6) and (7).

		$d_i$ [mm]	1.0	2.0	3.0	5.0	PH
Present method using	$L$ [mm]		3.9	15.4	34.7	96.4	105
Eqs. (6) and (7)	Volume ratio		0.043	0.17	0.39	1.03	1