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Abstract: The motions and added resistance of the S175 containership in regular head waves with different wave steepness under the same wave length are investigated using a Reynolds-averaged Navier-Stokes solver based on a finite-volume method. A level set method is used to capture the free surface and dynamic grids are adopted to simulate ship motions. The variation of heave and pitch motions and added resistance with the wave steepness agrees with the experiment. The higher harmonic components of surge force obtained by the Fourier analysis increase dramatically as the wave steepness increases while the higher harmonics of heave and pitch are quite small compared to the 1st harmonics even under large wave steepness. The transient pressure distributions are studied to explain the non-harmonic oscillations of the time history of resistance coefficient. The 0th, 1st, and 2nd harmonic amplitudes of pressure are plotted on the hull and the major part of resistance increase in steeper waves is found to be induced at the bow.

Keywords: added resistance, ship motions, wave steepness, RANS

1 Introduction

Added resistance in waves is one of the main components of the total resistance of ships in the actual sea states. Estimation of added resistance is important for the design of the propulsion system of a ship and for the prediction of the fuel consumption during actual operations. Recently, with the implementation of the IMO regulations about Energy Efficiency Design Index [1], added resistance calculation methods with higher precision are needed for the optimization of energy efficiency. Furthermore, the evaluation of added resistance in steep waves is essential for the calculation of Minimum Propulsion Power which is required in the IMO regulation [2]. Wave steepness has been proved to have a significant nonlinear influence on added resistance in the experiment [3] which shows that the added resistance coefficient in high waves is 18%~44% less than that of low waves. Therefore, wave steepness should be considered in the added resistance calculation methods and the influence of wave steepness should be investigated.

Nowadays, the conventional method to calculate added resistance is the potential flow method which can be categorized into the far-field method and the near-field method. In the far-field method, added resistance is evaluated based on the consideration of the energy and momentum relation in the far field. Early attempts to calculate added resistance were performed with a strip method [4-6]. With the development of 3D potential flow methods, the far-field formulation was applied with a 3D panel method [7, 8]. The near-field method, on the other hand, obtains added resistance by integrating the pressure on the hull surface. It can be carried out by means of a strip method [9], or a 3D panel method [10]. Recently,

the middle-field method, which obtains added resistance from a control surface near the hull, is introduced and added resistance can be estimated with the application of a Green Function panel method [11] or a Rankine Source panel method [12].

The potential flow method is established following the perturbation procedure, in which the boundary conditions are linearized based on the assumption of the small oscillations of boundaries. The added resistance problem is treated as a second-order problem and the added resistance obtained is proportional to the square of wave amplitude. Therefore, the potential flow method is theoretically valid for small wave steepness only. More comprehensive methods with different levels of complexity have been presented and modifications have been made to include nonlinear terms such as a nonlinear body condition, a nonlinear free surface condition, and a nonlinear wave model. However, these modifications are too complicated to be implemented in the calculation of added resistance. Recently, a simplified method to include the wave steepness in the added resistance calculation is presented by introducing the nonlinear wave excitation force [13]. Despite the continuous development of the potential flow method, due to the basic assumption of inviscid and irrotational flow, the potential flow method cannot be used to treat strongly nonlinear problems such as breaking waves which often happen in steep waves.

With the rapid development of CFD technique, the resistance of ships sailing in waves can be obtained through CFD simulations [14-17]. Extensive studies on seakeeping were carried out in the Gothenburg 2010 workshop [18]. A variety of CFD solvers with different turbulence models, free surface modeling methods, discretization methods, and grid types were adopted in these studies. In general, the CFD methods gave better results than the potential flow approaches. The motions and mean resistance fairly agreed with the experiment while large errors were observed for the 1st order harmonic amplitude of surge force. Most of the simulations were carried out under a series of wave frequencies and the influence of wave steepness was not examined except that Shen [19] evaluated the added resistance of the DTMB model 5512 with different wave steepness and strongly nonlinear features were observed. Compared to potential flow methods, CFD methods based on Navier-Stokes equations can deal with problems in steep waves and the flow details which help to understand the nonlinear features can also be obtained.

In this paper, the heave and pitch motion and added resistance for the S175 containership are calculated using a Reynolds-averaged Navier-Stokes (RANS) solver developed by Hino [20, 21]. The focus is the nonlinear behavior of the added resistance in steep waves, so the simulations are carried out at one wave length with a wide range of wave steepness. The calculated results for added resistance and ship motions are validated using the published experimental data. The higher order harmonic amplitudes are obtained by means of Fourier series to analyze the nonlinear characteristics. The pressure distributions on hull surface are studied to understand the non-harmonic oscillations of the resistance coefficient.

2 Numerical methods

The governing equations are the RANS equations with the introduction of artificial compressibility. With all variables non-dimensionalized by the reference length L_0 , reference velocity U_0 , and fluid density ρ_0 , the RANS equations can be expressed in the integral form as follows

$$\frac{d}{d\tau} \iiint_{\Omega} \mathbf{q} dV + \frac{d}{dt} \iiint_{\Omega} \mathbf{J} \mathbf{q} dV + \iint_{\partial\Omega} [(\tilde{\mathbf{e}} - \mathbf{e}^v) n_x + (\tilde{\mathbf{f}} - \mathbf{f}^v) n_y + (\tilde{\mathbf{g}} - \mathbf{g}^v) n_z] dS = 0 \quad (1)$$

where τ denotes the pseudo time and t denotes the physical time used in the dual time stepping described below. \mathbf{J} is a diagonal matrix defined as $\text{diag}(0,1,1,1)$. \mathbf{q} is the vector of the flow variables defined as

$$\mathbf{q} = \begin{bmatrix} p \\ u \\ v \\ w \end{bmatrix}$$

where (u, v, w) are the (x, y, z) components of the velocity of fluid and p is the modified pressure from which the hydrostatic component is extracted, i.e.,

$$p = p^* + \frac{z}{Fn^2} \quad (2)$$

where p^* is the original pressure and Fn is the Froude number defined as $U_0/\sqrt{gL_0}$. The inviscid fluxes $\tilde{\mathbf{e}}$, $\tilde{\mathbf{f}}$, and $\tilde{\mathbf{g}}$ are given by

$$[\tilde{\mathbf{e}} \quad \tilde{\mathbf{f}} \quad \tilde{\mathbf{g}}] = \begin{bmatrix} \beta u & \beta v & \beta w \\ u(u - u_g) + p & u(v - v_g) & u(w - w_g) \\ v(u - u_g) & v(v - v_g) + p & v(w - w_g) \\ w(u - u_g) & w(v - v_g) & w(w - w_g) + p \end{bmatrix} \quad (3)$$

where β is a parameter for artificial compressibility and (u_g, v_g, w_g) are the (x, y, z) components of the grid velocity of the surfaces S of the control volume V . The viscous fluxes \mathbf{e}^v , \mathbf{f}^v , and \mathbf{g}^v are given by

$$[\mathbf{e}^v \quad \mathbf{f}^v \quad \mathbf{g}^v] = \begin{bmatrix} 0 & 0 & 0 \\ \tau_{xx} & \tau_{xy} & \tau_{xz} \\ \tau_{yx} & \tau_{yy} & \tau_{yz} \\ \tau_{zx} & \tau_{zy} & \tau_{zz} \end{bmatrix} \quad (4)$$

where $\tau_{x_i x_j}$ ($i, j = 1, 2, 3$) is defined as

$$\tau_{x_i x_j} = \left(\frac{1}{Rn} + \nu_t \right) \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad (5)$$

where ν_t is the non-dimensional kinematic eddy viscosity and Rn is the Reynolds number defined as $U_0 L_0 / \nu$ where ν is the kinematic viscosity. ν_t can be obtained by a specific turbulence model. In the present work, $k - \omega$ SST turbulence model [22] is used except for the case with the largest wave steepness in which the $k - \omega$ SST turbulence model fails and the Spalart-Allmaras turbulence model [23] is used instead. The calculation results with two turbulence models for lower wave steepness are almost the same. So Spalart-Allmaras model is considered to be as accurate as $k - \omega$ SST in this study.

A finite volume method is adopted for spatial discretization [20]. The second-order upwind scheme is used for the inviscid flux and the second-order central difference scheme for the viscous flux. Velocity-pressure coupling is achieved based on the artificial compressibility concept in which the divergence free condition is satisfied in the steady state limit. To apply the artificial compressibility method to unsteady problems, dual time stepping [24] is adopted, in which pseudo time iterations are performed until the divergence free condition is satisfied at each physical time step. The second order two-step backward scheme and the first order Euler implicit scheme are used for the physical time stepping and pseudo time stepping, respectively. In the present study, the dual time stepping is used in simulations in incident waves. A calm water case is regarded as a steady problem in which only the pseudo time stepping is applied.

A level set method [21] is adopted to capture the free surface. In calm water conditions, to avoid the reflection of the free surface waves at the outer boundaries of the computational domain, a damping term is included in the solution. In wave conditions, the flow variables near the boundaries are set identical to the analytical formulation of the linear wave theory and they are blended with the inner flow field solved from the governing equations [25].

The motion equations are coupled with the dual time stepping through the 3rd order Adams-Bashforth/Adams-Moulton scheme [26]. The grids whose distance from the hull surface is

$0.3L_{pp} \sim 0.7L_{pp}$ are deformed at each time step fitting to the current position and attitude of the ship hull.

3 Geometry and simulation conditions

The S175 containership is used in the simulations because the experimental data under different wave steepness is available for this ship [3]. A ship model of a scale of 1:43.75 is used in the experiment and the same model is used in the simulation. Principal particulars of the S175 containership are listed in Table 1.

Table 1 Principal particulars of the S175 containership model

Parameters		Ship model
Length between perpendiculars	L_{pp} (m)	4.0000
Breadth	B (m)	0.5847
Draft at forward perpendicular (F.P.)	d_F (m)	0.1952
Draft at aft perpendicular (A.P.)	d_A (m)	0.2199
Displacement	∇ (m ³)	0.2769
Longi. center of buoyancy from F.P.	LCB (% L_{pp})	0.5200
Longi. radius of gyration	k_{yy} (% L_{pp})	0.2400
Height of C.G. above base line	KG (m)	0.1778

The freeboard is extruded vertically upward from the deck to increase the stability of simulations. This manner will eliminate the green water phenomenon in steep waves and cause calculation errors. However, the agreement with the experiment implies that the green water may have a small impact on the final results.

The simulation conditions are selected according to the experimental conditions. 5 cases in regular head waves and a calm water case are carried out. The Froude number Fn is set to 0.25 for all cases and the wave length λ is $0.9L_{pp}$ for the cases in waves. The ratio of wave height to wave length, H/λ , is 0.011, 0.022, 0.033, 0.044, and 0.056, respectively. The ship is free to heave, pitch, and surge in the experiment. However, the details of the spring system are unknown and the influence of surge motion is small [27,28]. So, the surge motion is ignored in the simulations.

4 Computational domain, boundary conditions, and grids

The computational domain is a rectangular domain shown in Figure 1. The domain is non-dimensionalized by L_{pp} . The origin of the coordinate system coincides with the forward perpendicular on the free surface and the x-axis is oriented from bow to stern. The y-axis is positive to star board with z-axis pointing upward. The computational domain extends from $-1.5 < x < 4.0$, $-2.0 < y < 0.0$, and $-2.0 < z < 0.2$ for all cases. The no-slip boundary condition is applied on the hull surface and the symmetry condition is imposed on $y=0$. For the inlet, the inflow velocity is specified and for the outlet, top, side, and bottom, the pressure and the velocity are extrapolated except that the pressure is specified on the outlet boundary.

In the calm water condition, the wave damping zone shown in Figure 2 is set at the inlet, side, and outlet to avoid the reflection of waves. The width of the wave damping zone is 0.5. In wave conditions, the flow variables are set identical to the analytical solution for linear waves in the wave generating zone shown in Figure 3 and they are blended gradually with the inner flow field in the blending zone. The width of the wave generating zone and blending zone is both 0.25.

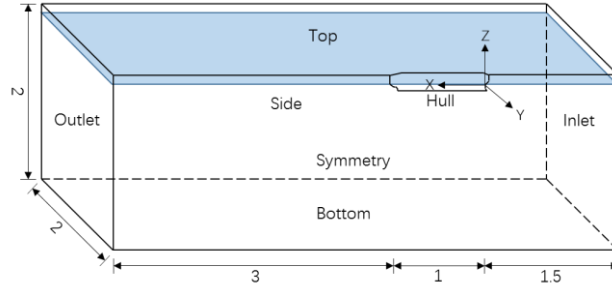


Figure 1 Computational domain

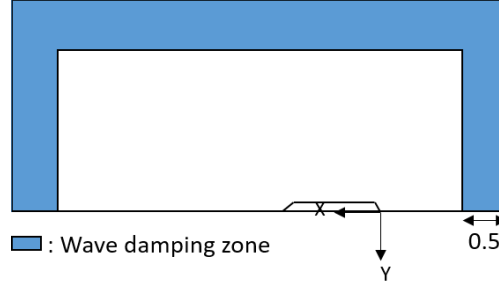


Figure 2 Wave damping zone viewed from top

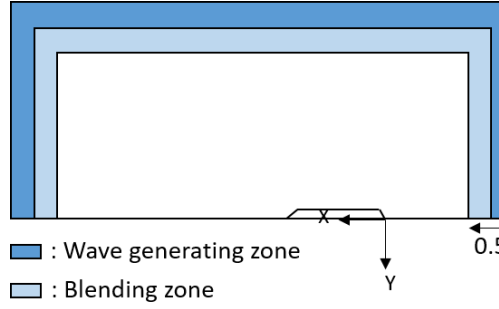


Figure 3 Wave generating zone and blending zone viewed from top

Unstructured hexahedral grids are used in the present study and boundary layer grids are generated on the hull surface with the minimum spacing on the wall being 5×10^{-6} . Grid refinement is required near the free surface and in the Kelvin wave region to resolve the incident waves and the ship generated waves well. The grids are also refined near the hull to obtain the flow details.

The grid size of the flow field is determined by the requirement of the incident wave modeling. The wave height usually reduces gradually as waves propagate due to numerical dissipation. The decay rate of waves is relevant to the grid size near the free surface. To obtain the suitable grid size, a series of grid-dependence tests are performed. In these simulations, the ship hull is extracted from the computational domain and the dimension in y direction is reduced to save the computing time while keeping the same in x and z direction. The other parameters for simulations are $Fn = 0.25$, $\lambda = 0.9L_{pp}$, and $H = 0.033\lambda$.

The results are shown in Table 2. λ/dx and H/dz denote the subdivisions of wave length and wave height, which means how many cells are divided into in one wave length and one wave height. H'/H denotes the ratio between the simulated wave height measured at the aft perpendicular and the desired wave height which is an input parameter. The results indicate that wave decay is more sensitive to the subdivision of wave length and the decay rate is much slower with a denser subdivision of wave length. The subdivision of wave height makes smaller differences on the results compared to wave length.

Table 2 Results of grid-dependence tests for incident wave modeling

Case NO.	λ/dx	H/dz	H'/H
1	100	10	0.7219
2	100	20	0.7303
3	150	10	0.8598
4	150	20	0.8695
5	200	5	0.8557
6	200	10	0.9036
7	200	20	0.9142

$\lambda/dx = 200$ and $H/dz = 10$ are used in the following simulations out of the consideration of the balance between accuracy and efficiency. $H/dz = 10$ is kept for all wave cases, which means that the height of grids varies with wave height. The grids viewed from three directions for the case $H = 0.033\lambda$ is shown in Figure 4, Figure 5, and Figure 6, respectively. As shown in Figure 4, $\lambda/dx = 200$ is applied in front of the ship, along with the ship, and down to one ship length behind the ship. Behind that $\lambda/dx = 100$ is used because the wave propagation downstream of the ship has less influence on the issues concerned. Besides, the grid refinement mentioned above is observed in the Kelvin wave region and very fine grids can also be observed near the free surface and hull surface in Figure 5 and Figure 6.

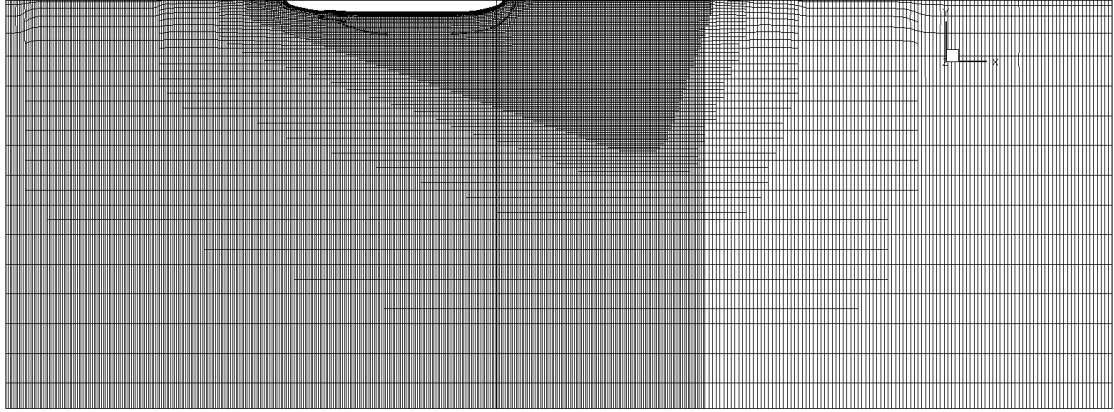


Figure 4 Grids of slice located at $z=0.07$

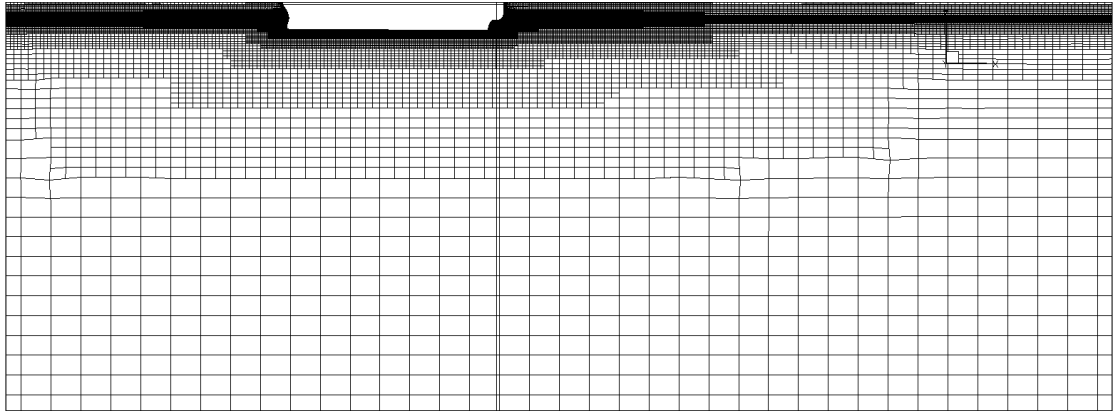


Figure 5 Grids of slice located at $y=0$

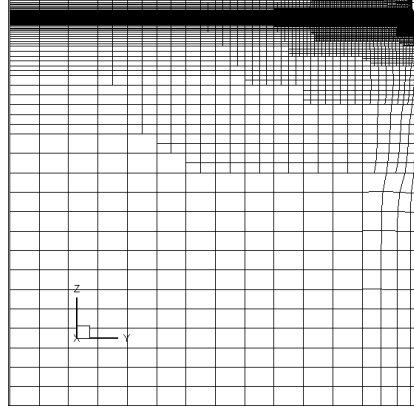


Figure 6 Grids of slice located at $x=1$

5 Results and discussions

Time histories of wave elevation, ship motions, and resistance coefficient

The total simulation time is $15T_e$ where T_e is the encounter period. After about $5T_e$, the system reaches a steady periodically changing state. Time histories of wave elevation, heave, pitch, and resistance coefficient in one encounter period are shown in Figure 7. Wave elevation ζ and heave motion ξ_3 are non-dimensionalized by Lpp . Pitch motion ξ_5 is expressed in rad. The resistance coefficient C_t is defined as

$$C_t = F_x / (0.5\rho U^2 Lpp^2) \quad (6)$$

where F_x is the measured external force of the ship in x direction (the total resistance of the ship). Note that the time history of the wave elevation is recorded at a point which has the same x coordinate as F.P. but shifts $1.0Lpp$ away from $y=0$ in y direction, so that the disturbance caused by the ship can be neglected.

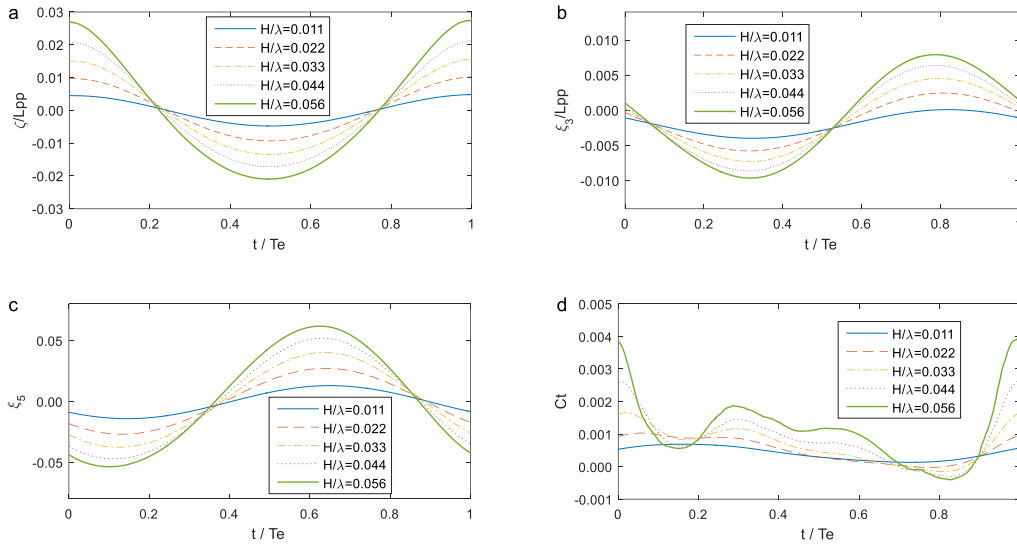


Figure 7 Time histories in one encounter period. a wave elevation, b heave, c pitch, d resistance coefficient

For heave and pitch, harmonic oscillations with the period conforming to those of incident waves are observed. For resistance coefficient, the oscillations are harmonic approximately only for the case with the smallest wave steepness. Nonlinear characteristics arise and are enhanced with the increase of wave steepness.

Computation of mean value

The results shown in Figure 7 are analyzed by means of Fourier series. n^{th} ($n \geq 0$) harmonic amplitudes of ζ , ξ_3 , ξ_5 , and F_x will be denoted as $\zeta^{(n)}$, $\xi_3^{(n)}$, $\xi_5^{(n)}$, and $F_x^{(n)}$. $F_x^{(0)}$ represents the mean resistance in waves and $F_x^{(n)}$ ($n \geq 1$) represents the n^{th} harmonic amplitude of the surge exciting force.

It is found that the mean value cannot be evaluated precisely by means of Fourier series in one period, especially under small wave steepness. Figure 8 (a) shows the time histories of wave elevation, heave, pitch, and resistance coefficient for the case $H/\lambda = 0.011$. After a transition phase in which the waves propagate to the measurement point, the wave elevation begins to vary periodically. However, there is a low frequency disturbance whose period is about 5~6 times of the wave period due to numerical error. It induces the low frequency variation of heave, pitch, and especially the resistance coefficient, which is more sensitive to wave elevation and also influenced by ship motions. Then the computation of $F_x^{(0)}$ will depend on the selection of the time window, in which F_x is time-averaged. The low frequency oscillations also exist for larger wave steepness as shown in Figure 8 (b). However, as the wave steepness increases, the amplitudes of wave elevation, motions, and resistance coefficient also increase and the influence of low frequency oscillation is relatively small. The grid-dependence tests show that the low frequency component cannot be eliminated by increasing the number of the mesh but it will gradually decay with time going on. However, it will cost too much time when the low frequency oscillation finally vanishes.

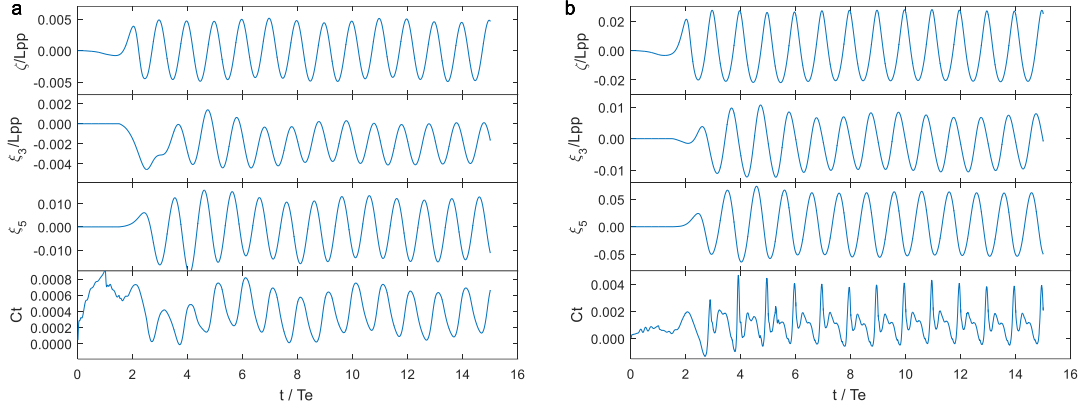


Figure 8 Time histories of wave elevation, heave, pitch, and resistance coefficient. a $H/\lambda = 0.011$, b $H/\lambda = 0.056$

To reduce the error caused by the low frequency oscillation, $F_x^{(0)}$ is determined in the following way. $F_x^{(0)}$ computed from the time window whose length is one encounter period is plotted in Figure 9, in which t_1 represents the start point of the time window. t_1 is selected at every time instant while the length of the time window keeps the same. The curve can be approximated as a function in the following form

$$F_x^{(0)} = a + be^{-c} \cos\left(\frac{2\pi}{d}t_1 + e\right) \quad (7)$$

in which a , b , c , d , and e are determined by nonlinear least squares method. The fitted curve is also plotted in Figure 9. $F_x^{(0)}$ is assumed to follow the trend of the fitted curve with time going on. The fitted curve will finally converge at the coefficient a , which is the mean resistance expected. Because the form of the fitted curve is assumed based on the time history of $10 T_e$ which is not long enough, there is still some error caused by low frequency oscillation. However, this method can reduce the error to a great

extent.

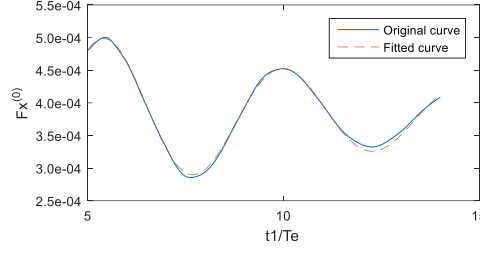


Figure 9 Variation of $F_x^{(0)}$ with the start point of time window

Validation of the computational results

The results of the non-dimensional 1st harmonic amplitudes of heave and pitch and the added resistance coefficient are shown in Figure 10. The horizontal axis represents the actual wave steepness defined as H'/λ where H' represents the measured wave height defined as $2\zeta^{(1)}$. H' should be distinguished from H which is an input parameter of the simulation. The non-dimensional 1st harmonic amplitudes of heave and pitch will be non-dimensionalized by $\zeta^{(1)}$ and $k\zeta^{(1)}$, where k is the wave number. Added resistance R_{AW} is calculated by

$$R_{AW} = F_x^{(0)} - F_x^{(Calm)} \quad (8)$$

where $F_x^{(Calm)}$ represents the calm water resistance which is computed using the same CFD method. The added resistance coefficient is defined as

$$C_{AW} = R_{AW} / (\rho g (\zeta^{(1)})^2 B^2 / Lpp) \quad (9)$$

Both the computational and experimental results for the non-dimensional 1st harmonic amplitudes of heave and pitch and the added resistance coefficient show a decreasing trend with the increase of wave steepness and the matching between calculation and experiment is quite satisfying. It indicates that the present CFD method has the capability to calculate motions and resistance of ships in steep waves and the influence of wave steepness can be considered effectively. It should be noted that the trends of ship motions and added resistance may be frequency dependent and the trends may be different at other frequencies.

Besides the difference of amplitude of heave and pitch shown in Figure 10, there is also difference of phase among cases with different wave steepness. The phase lags between 1st harmonics of ship motions and 1st harmonics of wave elevation at F.P. are plotted in Figure 11 and a difference about 10 deg can be observed for the phase lags. However, there is no experimental data about the phase.

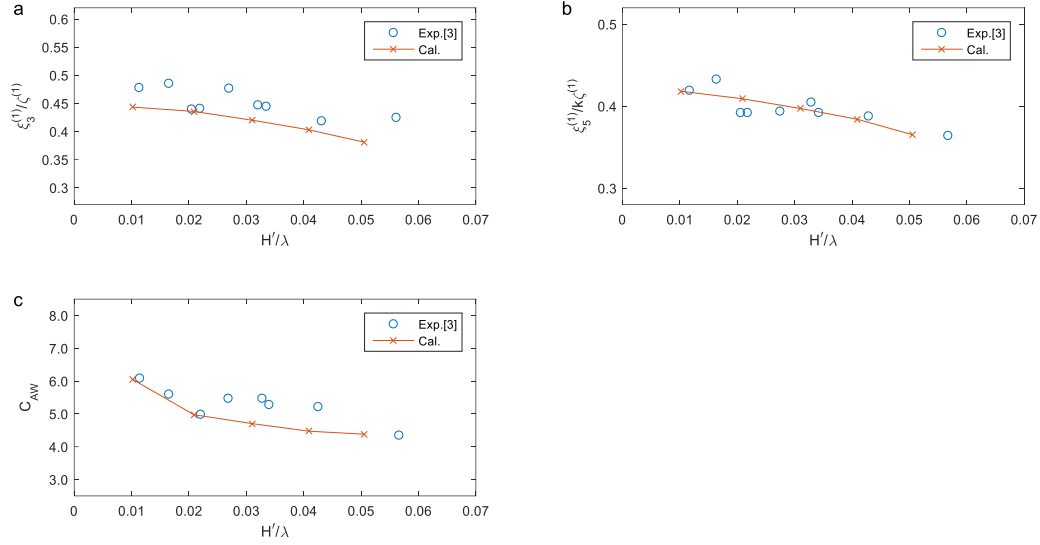


Figure 10 Comparison with the experimental data. a non-dimensional 1st harmonic amplitudes of heave, b non-dimensional 1st harmonic amplitudes of pitch, c added resistance coefficient

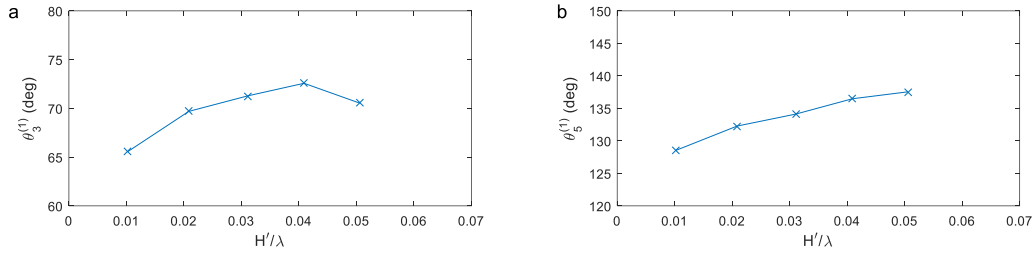


Figure 11 Phase lags between 1st harmonics of ship motions and 1st harmonics of wave elevation at F.P. a heave, b pitch

Higher harmonic components

The higher harmonic behaviors are analyzed by comparing higher harmonic amplitudes with the 1st harmonic amplitudes. The results for heave, pitch, and surge force are shown in Figure 12. The higher harmonic amplitudes for heave and pitch are significantly smaller than the 1st harmonics even in the highest waves. For the surge force, the higher harmonic amplitudes are small compared to the 1st harmonics only in cases with the smallest wave steepness. The higher harmonic amplitudes increase rapidly as the wave steepness grows. The 2nd and 3rd harmonic amplitudes are even larger than the 1st harmonic amplitude in the largest wave steepness case. The 3rd harmonic component is smaller than the 2nd harmonics only under the smallest wave steepness. For cases with larger wave steepness, the 3rd harmonic amplitude is almost the same as the 2nd harmonics.

The potential flow method to calculate added resistance is established based on the assumption of a small steepness of incident waves. A perturbation solution in terms of this small parameter is adopted to obtain the surge force of different orders. The 2nd and 3rd harmonic surge forces are regarded as higher order small values and should be much smaller than the 1st harmonic. However, the simulation results show that the amplitudes of the 2nd and 3rd harmonic surge forces are almost as large as the 1st harmonic in cases with large wave steepness. Such nonlinearity may be beyond the scope of the perturbation solution adopted in the potential flow method.

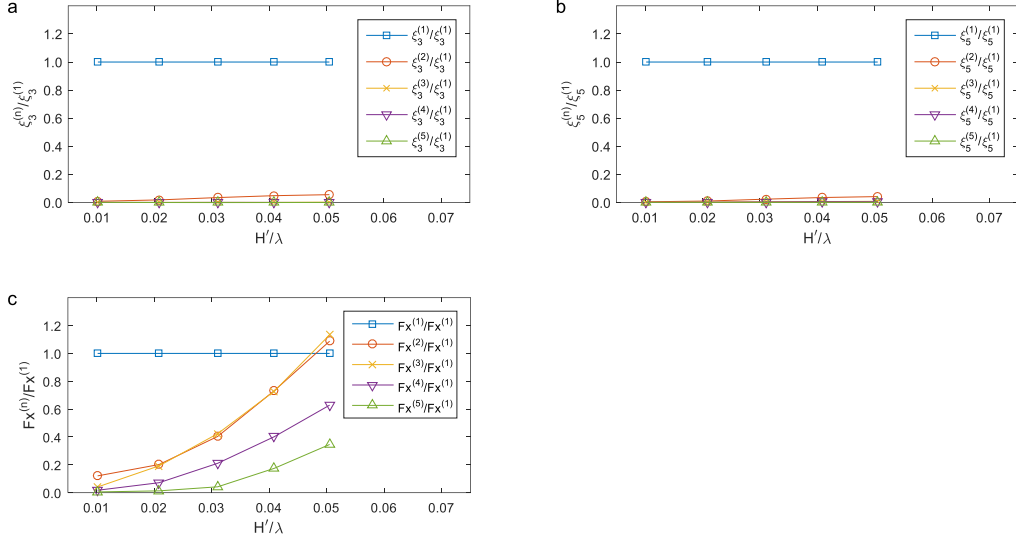


Figure 12 The ratio of higher harmonic amplitudes and 1st harmonic amplitude. a heave, b pitch, c surge force

Pressure distribution

To explain the non-harmonic variations of the time history of resistance coefficient, the pressure distribution at each time step is studied. First, time histories of wave elevation, heave, pitch, and resistance coefficient for the case $H/\lambda = 0.056$ in one encounter period are drawn in Figure 13. Noted that the time history of wave elevation is recorded at a point which has the same x coordinate as the F.P. but shifts $1.0L_{pp}$ away from the F.P. in y direction. The start time of one period is selected in the way that the wave crest is located at the F.P. at $t/T_e = 0$.

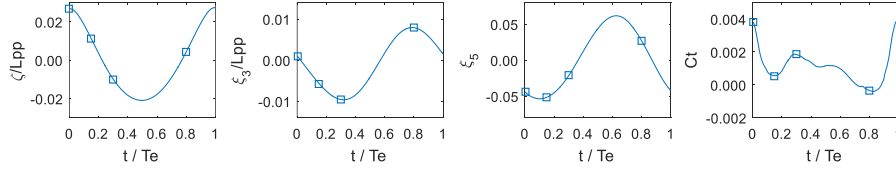


Figure 13 Time histories of wave elevation, heave, pitch, and resistance coefficient in one encounter period

Resistance coefficient reaches its maximum at $t/T_e \approx 0$ and minimum at $t/T_e \approx 0.8$. Also, there is a local minimum at $t/T_e \approx 0.15$ and a local maximum at $t/T_e \approx 0.3$. The pressure distributions on the hull surface for these time steps are drawn in Figure 14. The contour represents the x component of the pressure p^* in equation (2). The bold curve in blue color near the free surface is the wave profile on the hull. Figure 15 shows the resistance distribution along the ship. F_x is the x component of the integral of the pressure p^* along each section. The horizontal axis represents the x coordinate of each section.

At $t/T_e \approx 0$, the wave crest is located at the bow and the pitch is approaching the maximum bow-down. Very high pressure is observed at the bow in Figure 14. The high pressure and large immersed area at the bow make significant contribution to the resistance which can be confirmed in Figure 15. At $t/T_e \approx 0.15$, a local minimum value occurs. As shown in Figure 14, the wave crest moves a little towards the stern and the pressure at the bow decreases significantly compared to $t/T_e \approx 0$. At $t/T_e \approx 0.3$, the resistance coefficient reaches a local maximum value. The wave crest continues to move to stern and the

downward heave maximum is reached (see Figure 13) which means the largest area of wetted surface can be expected. The minimum value of resistance is obtained at $t/T_e \approx 0.8$ which is correspond to the largest upward heave motion (see Figure 13). It is shown in Figure 14 that very small hull surface immerses in the water and no obvious high-pressure region is observed. This causes the minimum resistance.

To summarize, the non-harmonic fluctuations of the time history of the resistance coefficient result from the nonlinear interactions between ship motions and waves. The pressure on the wetted surface varies dramatically both in space and time, especially near the bow. The wetted surface also changes violently as a result of the wave propagation and ship motions. The phase difference between ship motions and incident waves plays an important role.

According to the perturbation solution adopted in the potential flow theory, the variation of wetted hull surface should be small. Then only the velocity potential on the mean wetted hull surface needs to be solved and the influence of the hull shape above the mean waterline cannot be considered. However, the visualization of the wave profile on the hull shows that the variation of wetted surface is so violent that the influence of the flare shape cannot be ignored. There is also other strongly nonlinear phenomenon which cannot be considered in the potential flow theory, such as the breaking waves at the bow. The conventional potential method cannot consider these factors and may give inaccurate prediction of added resistance under large wave steepness. More precise methods, such as the present method, are needed to solve these problems.

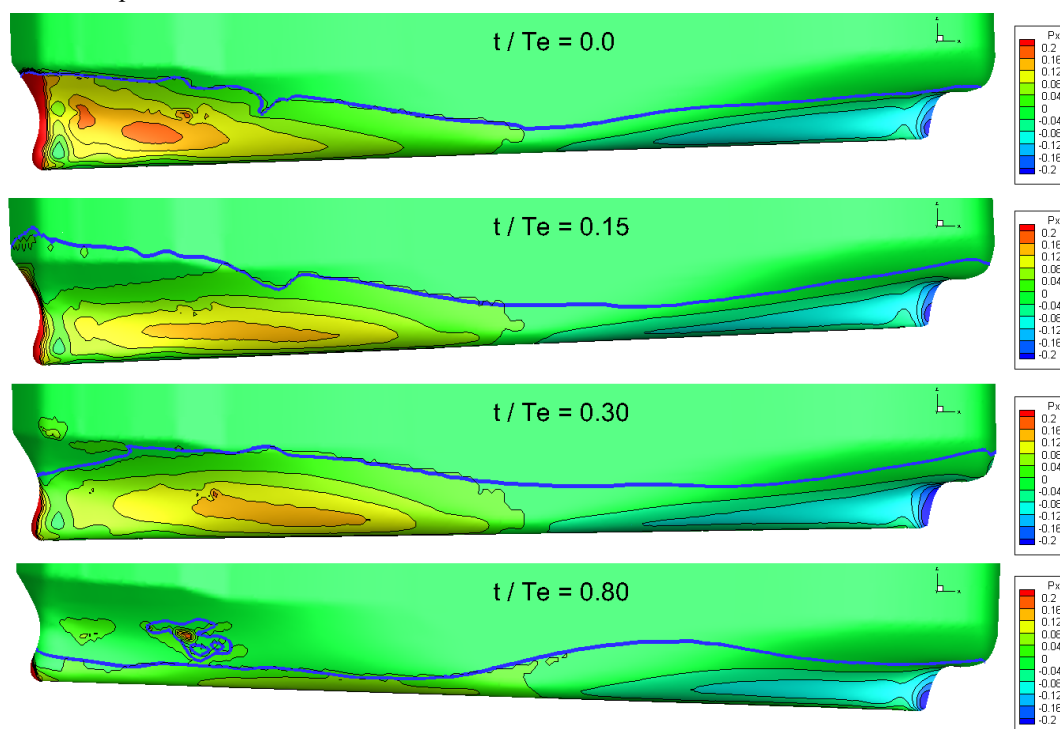


Figure 14 X component of pressure at $t/T_e = 0, 0.15, 0.3, 0.8$ for the case $H/\lambda = 0.056$

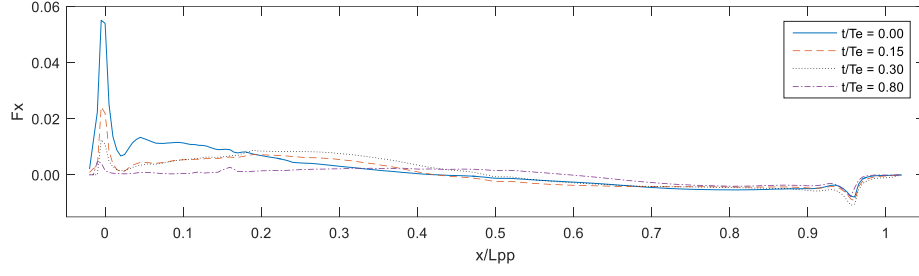


Figure 15 Resistance distributions along x axis at $t/T_e = 0, 0.15, 0.3, 0.8$ for the case $H/\lambda = 0.056$

Figure 16 shows the time-averaged x component of pressure for the calm water case and three cases in waves. Figure 17 shows the time-averaged resistance distributions along x axis. \bar{F}_x represents the time-averaged value of F_x in one period. It can be observed in Figure 16 that the high-pressure area near the bow become larger gradually with the increase of wave steepness. In Figure 17, four curves are almost coincident except in the region of $x/Lpp < 0.2$ and $0.5 < x/Lpp < 0.7$. The most significant difference is found at the positive peak near the bow. These results indicate that the major part of resistance increase in steeper waves is induced near the bow. Figure 18 and Figure 19 show the 1st and 2nd harmonic amplitudes of the x component of pressure for the case of $H/\lambda = 0.011, 0.033, 0.056$. With the increase of wave steepness, both 1st and 2nd harmonic amplitudes increase, especially near the bow.

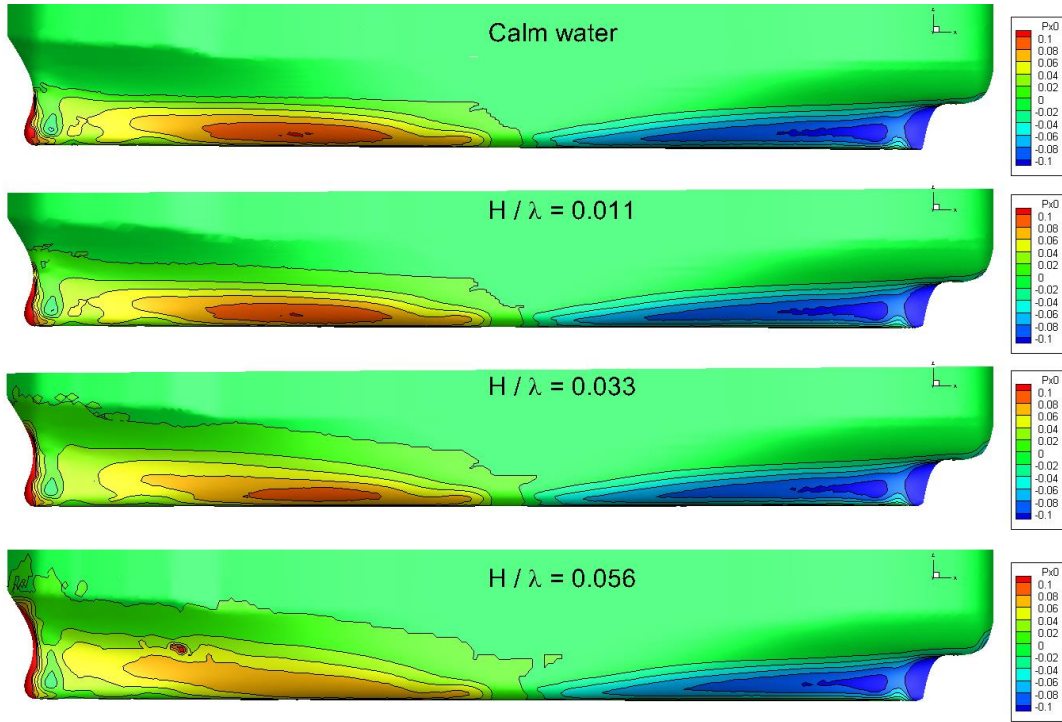


Figure 16 Time-averaged x component of pressure for the calm water case and three cases in waves ($H/\lambda = 0.011, 0.033, 0.056$)

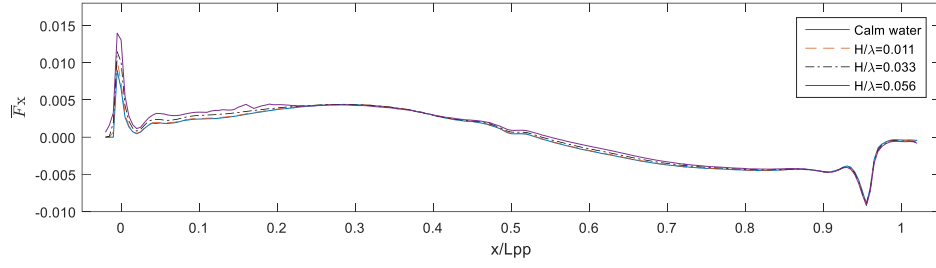


Figure 17 Time-averaged resistance distributions along x axis for the calm water case and three cases in waves ($H/\lambda = 0.011, 0.033, 0.056$)

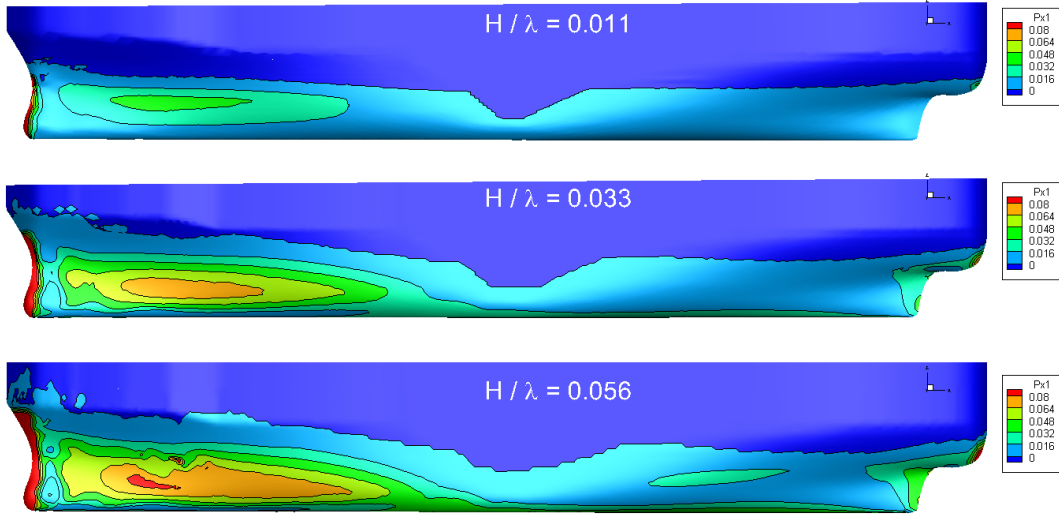


Figure 18 1st harmonic amplitude of the x component of pressure for the case $H/\lambda = 0.011, 0.033, 0.056$

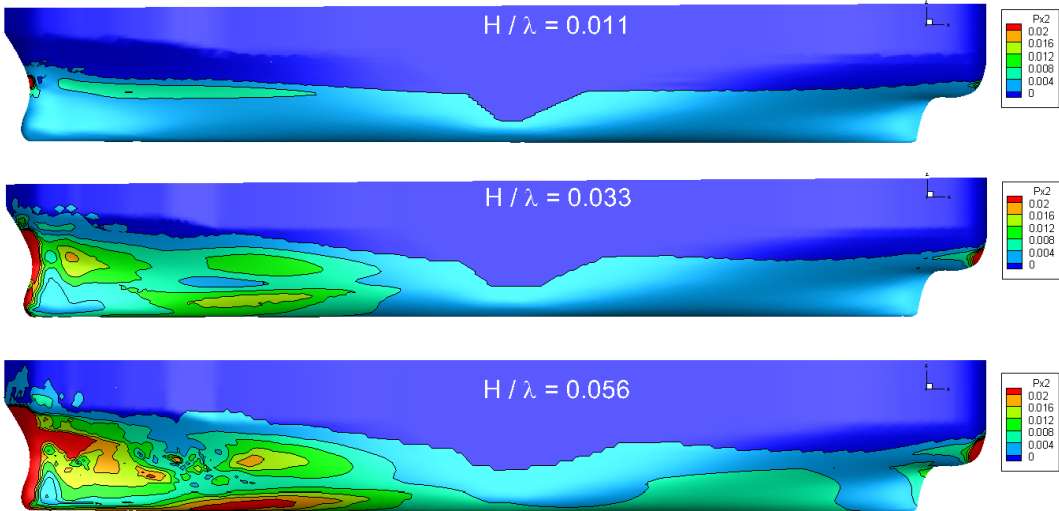


Figure 19 2nd harmonic amplitude of the x component of pressure for the case of $H/\lambda = 0.011, 0.033, 0.056$

6 Conclusions

Ship motions and added resistance of the S175 containership under different wave steepness at a fixed wave length are calculated by a RANS solver based on a finite volume method in an unstructured grid. A level set function is employed to capture the free surface and ship motions are considered with the application of dynamic grids. The grid-dependence tests are performed to investigate the influence of grid size on the quality of incident wave propagation.

The non-dimensional amplitudes of heave and pitch and added resistance coefficients under different wave steepness agree well with the experimental data. This indicates that the present numerical method can take into account the influence of wave steepness with good accuracy.

It is shown that the higher harmonic components of surge motion increase dramatically as the wave steepness increases which indicates the limitation of the application of 2nd order potential flow theory in high waves. For heave and pitch motion, higher harmonics are quite small compared to the 1st harmonics.

Very complicated transient wave patterns and hull pressure distributions are observed. The nonlinearity of resistance is closely related to the amplitude and phase of incident waves and ship motions and the interactions between them. The 0th, 1st, and 2nd harmonic amplitudes of pressure are plotted on the hull and the major part of resistance increase in steeper waves is found to be induced at the bow.

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